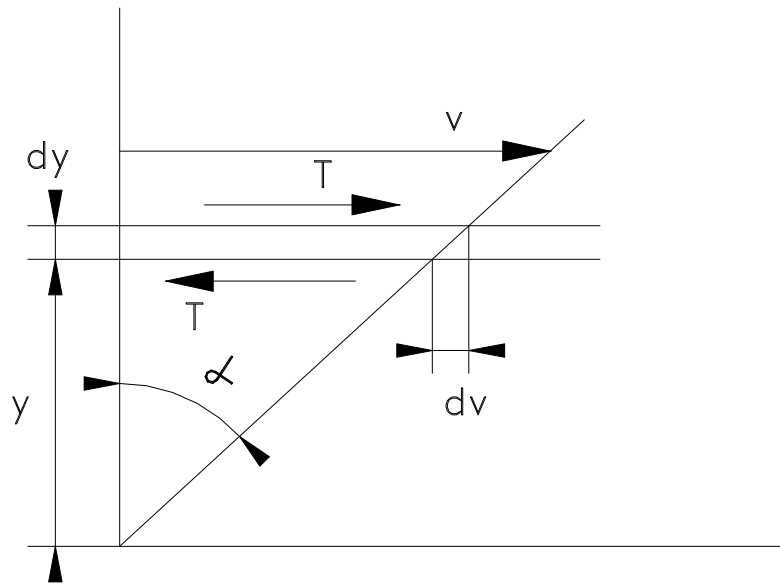


Air-viscosity / Reynolds-number



$$\text{Shearstress : } \frac{T}{A} = \tau = \eta * \frac{dv}{dy} \quad (\text{Stokes law})$$

τ = material-constant * velocity-gradient

η = viscosity : dimension : $\text{N/m}^2 * \text{m/m}/(\text{sec}) = \text{Ns/m}^2$

$\nu = \eta/\rho(\text{air}) = \text{dynamic viscosity} :$ dimension : $\text{Ns/m}^2/(\text{kg/m}^3) = \text{Nsm/kg}$

Under the circumstances where the gas behaves as an ideal gas, η can be considered as independent of the pressure.

In pneumatic conveying, the pressures are so low that this is permissible.

The dependency of temperature is given by :

$$\eta = \eta_0 * \sqrt{\frac{T}{T_0} * \frac{(1-c/T_0)}{(1+c/T)}}$$

for air :

$$\eta_0 = 1.72 * 10^{-5} \text{ Ns/m}^2$$

$$T_0 = 273 \text{ }^\circ\text{K}$$

$$c = 113$$

for nitrogen :

$$\eta_0 = 1.67 * 10^{-5} \text{ Ns/m}^2$$

$$T_0 = 273 \text{ }^\circ\text{K}$$

$$c = 100.8$$

i.e. :

$$\text{air at } 20 \text{ }^\circ\text{C} \quad \eta = 1.8 * 10^{-5} \text{ Ns/m}^2$$

Derivation of Reynolds-number

Method : prototype-/model comparison
 p = prototype
 m = model

$$L_p = c_l * L_m \quad (\text{length})$$

$$v_p = c_v * v_m \quad (\text{velocity})$$

$$\rho_p = c_\rho * \rho_m \quad (\text{density})$$

$$\eta_p = c_\eta * \eta_m \quad (\text{viscosity})$$

$$g_p = c_g * g_m \quad (\text{gravitational acceleration})$$

$$\zeta_p = c_\zeta * \zeta_m \quad (\text{resistance due to roughness})$$

Resistance of prototype :

$$W_p = \eta_p * dv_p/dy_p * A_p$$

Resistance of model :

$$W_m = \eta_m * dv_m/dy_m * A_m$$

Substituted :

$$W_p = c_\eta * c_v/c_l * c_l^2 * \eta_m * dv_m/dy_m * A_m$$

$$W_p = c_\eta * c_v * c_l * W_m$$

Also :

$$W_p = 1/2 * \zeta_p * \rho_p * v_p^2 * A_p$$

$$W_m = 1/2 * \zeta_m * \rho_m * v_m^2 * A_m$$

Substituted :

$$W_p = c_\zeta * c_\rho * c_v^2 * c_l^2 * W_m$$

Result in :

$$c_\eta * c_v * c_l = c_\zeta * c_\rho * c_v^2 * c_l^2$$

For $c_\zeta = 1$ (Equal roughness for prototype and model)

$$(c_\rho * c_v * c_l)/c_\eta = 1$$

$$\rho_p/\rho_m * v_p/v_m * L_p/L_m * \eta_m/\eta_p = 1$$

or :

$$\frac{\rho_p * v_p * L_p}{\eta_p} = \frac{\rho_m * v_m * L_m}{\eta_m}$$

In case the value : $\frac{\rho * v * L}{H}$

is equal for model and prototype , the scaling-factors are applicable for both situations.

This ,because the flows are comparable regarding friction-forces.

Reynoldsnumber : $\mathbf{Re} = \frac{\rho * v * L}{\eta}$

or :

$$\mathbf{Re} = \frac{v * L}{\nu}$$

in which :

$$\nu = \eta/\rho$$